

AGC of Solar-Thermal System Using Cuttlefish Optimization Algorithm under Deregulated Environment

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Abstract: Maintaining frequency stability in modern power systems is a critical challenge, especially in deregulated environments where diverse generating sources, such as renewable and conventional units, operate under market-driven conditions. In this study, a Tilt Integral Derivative (TID) controller is proposed for Automatic Generation Control (AGC) in a multi-area power system integrating solar-thermal units. The primary objective is to enhance system stability while accounting for key nonlinearities, such as Generation Rate Constraints (GRCs) and Governor Dead Band (GDB), which significantly affect dynamic performance. To optimally tune the TID controller parameters, we employ the Cuttlefish Optimization Algorithm (COA), a novel bio-inspired optimization approach. The effectiveness of the COA-based TID controller is assessed by comparing its performance with other established optimization techniques, including the Grey Wolf Optimization (GWO) algorithm. Key performance metrics, such as peak overshoot (PO), peaks undershoot (PU), and settling time (ST), are analyzed under varying load disturbances. Simulation results demonstrate that the COA-optimized TID controller outperforms competing methods, providing superior frequency stability, faster response times, and reduced oscillations in an open-market power system. The findings establish COA as a robust alternative for AGC tuning, particularly in systems with high renewable energy penetration and deregulated operation.

Keywords: TID controller; Automatic Generation and Control; Deregulation; Cuttlefish Optimization Algorithm; DISCO participation matrix.

1. Introduction

Frequency is a critical aspect of power systems. Recently, the frequency of regulation in power systems has often enchanted research concerns. Every power plant needs to keep an eye on how much energy is consumed during the day sorted out to match the ever-rising constraints of its customers for excellent service. Because there is never a steady energy source, load disturbances are used to reduce power fluctuations at different times of the day. Under the current conditions, it is essential to guarantee a consistent and affordable electrical supply while effectively distributing power through a connected device consistently and affordably. Load disturbances significantly impact machine power supply frequency, while reactive power exhibits variable responses to changes in voltage and current conditions.

Moreover, the community's structure will get increasingly complex as more sites are linked together through the process of linking traces. The magnetizing current will persist to increase in strength, even with a little decrease in frequency. Both the transformer and the coil may experience exhaustion or fatigue due to the increasing electrical current passing through it. In the current setting, it is difficult to maintain a steady electric system due to the increased power consumption. During operation, electrical equipment has a continuous change in weight. This device's principal task is to guarantee the necessary level of stability and robustness in the electrical machinery. The generator's mechanical output strain is inversely correlated with the tool's frequency[1-4].

The concept of frequency regulation encompasses three separate levels, namely primary, secondary, and tertiary. The primary frequency control loop detects a decrease in frequency prior to the activation of the relays that protect against under/over frequency. The utilization of the governor droop is a common practice in primary frequency control, resulting in chronically recorded inaccuracies. The regulation of frequency in power systems is the responsibility of secondary frequency control, which is also referred to as AGC or LFC. The main goals of this system are to maintain the frequency within a specified range and to effectively regulate the transmission of power between control regions through significant tie lines [5-7].

The primary target of the single-area LFC system is to achieve control over the operating frequency, ensuring that it remains at its nominal value without requiring any adjustments to the interconnected system. To achieve load balancing in a multi-area load factor correction (LFC) system, it is necessary for the generators in each area to effectively handle both the local load and the power fluctuations on the tie lines that connect several regions [8-10]. The frequency management method entails the integration of the ACE signal into the feedback loop. This approach not only considers fluctuations in voltage and frequency transfer but also addresses the mistakes in energy and time resulting from irregularities in schedules and devices [11-13].

The Genetic Algorithm (GA) is employed to optimise data by adjusting the parameters of a discrete PI controller [14]. A graphical method is used to tweak the proportional-integral (PI) controller settings for a single-area LFC system with a time delay in order to achieve stability. A crucial aspect of the technique is the determination of the stability boundary locus. The validity and efficacy of the recommended technique are demonstrated using time-domain simulations. The stability region is depicted within the parameter space of the controller [15]. Fuzzy gain scheduling of PI controllers is employed for load frequency management in multi-power systems [16-17]. The performance of LFCs is influenced by nonlinear parameters such as the GDB and GRC [18-19]. Various methodologies, including as Firefly, HGS and COA, have been examined to enhance controller configurations [20-22]. The management of AGC in multi-area systems is facilitated through the utilization of a PID controller [23-24]. In multi-area systems, the management of AGC is facilitated through the utilization of a TID controller [25-27].

2. Multi Area Power System

The AGC system consists of two power plants: a thermal unit and a solar unit, as depicted in Figure 1, each consisting of two GENCOs and DISCOMS.

A. Conventional Electric power system scenario

The conventional electricity market comprises utilities that possess and manage their own power infrastructure. The public service exercises complete control over every aspect of production and delivery. Utilities possess and control the infrastructure and electrical lines, which they directly sell to consumers. Utilities are required to adhere to the electricity pricing established by the state utility council. This market is commonly referred to as a monopoly because it offers limited options for consumers. Nevertheless, its benefits encompass consistent pricing and enduring stability.

B. Deregulated power system scenario

Deregulation, as applied within the electrical sector, refers to the procedure of amending the governing rules and regulations to increase the number of energy providers available to consumers. Customers and energy dealers are permitted to allocate their funds as they see appropriate toward the expansion and maintenance of electricity transmission and generation systems in a deregulated electrical zone. A significant portion of the electricity generated by the Genco assets is distributed through retail utility infrastructure. The capacity to evaluate and contrast costs and services, in addition to the implementation of probability-based methodologies, are both advantageous for customers.

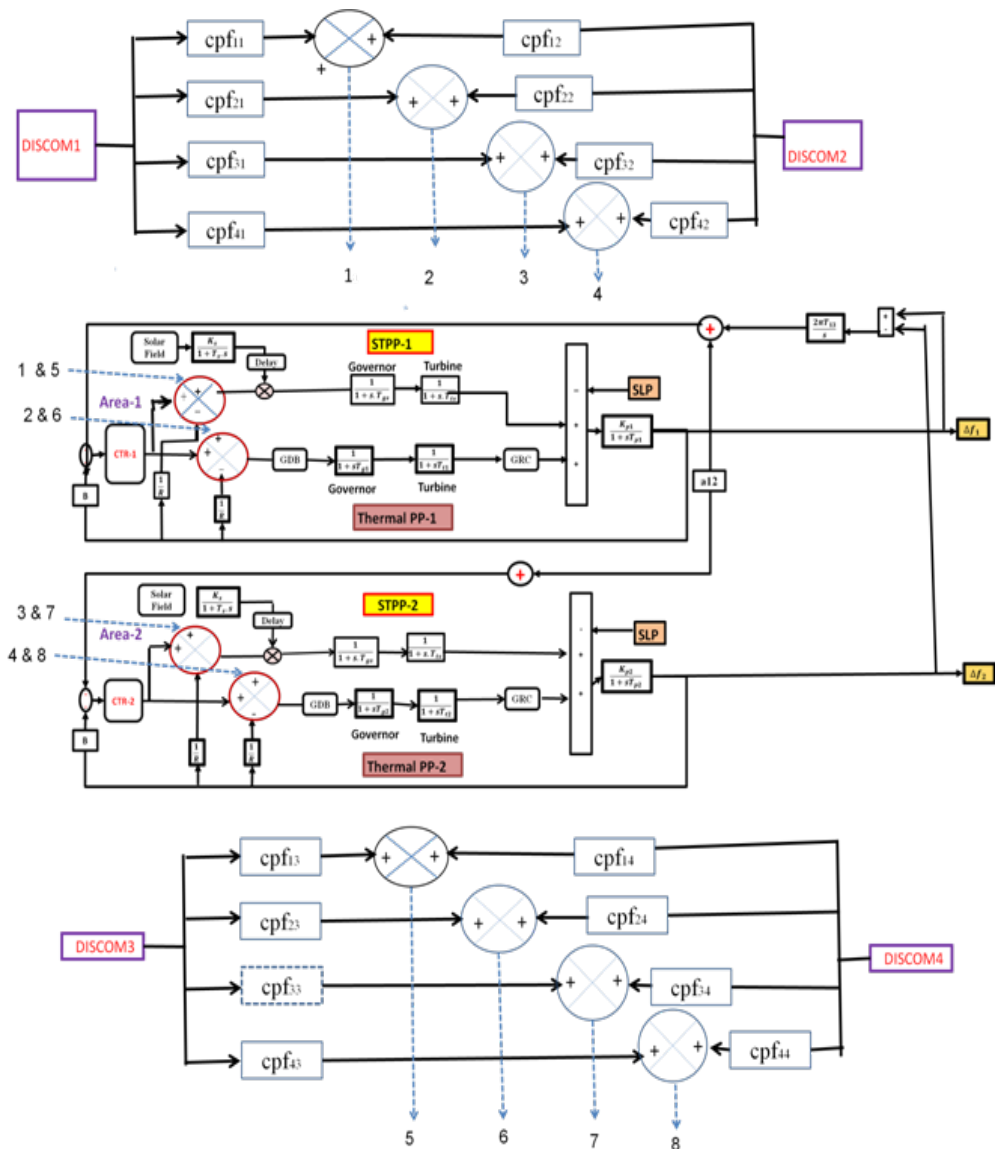


Figure 1. Two area Solar-Thermal restructured power system block diagram

$$\Delta P_{tie1-2,scheduled} = (\text{Total required load of Disco's in second area from first area in the Genco's}) - (\text{Total required load of Disco's in first area from second area in the Genco's}) \quad (1)$$

$$\Delta P_{tie1-2,scheduled} = \Delta P_{tie1-2,error} + \Delta P_{tie1-2,actual} \quad (2)$$

$$e_1(t) = ACE_1 = B_1 \Delta f_1 + \Delta P_{tie1-2,error} \quad (3)$$

$$e_2(t) = ACE_2 = B_2 \Delta f_2 + \Delta P_{tie2-1,error} \quad (4)$$

C. Disco Participation Matrix (DPM)

Each column in the DPM must have a total value of unity for Genco to provide the required load to the disco regardless of the region or condition.

$$DPM = \begin{bmatrix} cpf_{11} & cpf_{12} & cpf_{13} & cpf_{14} \\ cpf_{21} & cpf_{22} & cpf_{23} & cpf_{24} \\ cpf_{31} & cpf_{32} & cpf_{33} & cpf_{34} \\ cpf_{41} & cpf_{42} & cpf_{43} & cpf_{44} \end{bmatrix}$$

3. Design of Controllers

A. TID Controller

TID controllers exhibit similarities to PID controllers as they both incorporate A tilting component with a transfer function of $S^{-(1/n)}$ will be employed as the substitute for the proportional component of the controller. Figure 2 depicts the block diagram of the TID controller.

$$T.F (TID) = K_T (1/s)^n + K_I/S + K_D S \quad (5)$$

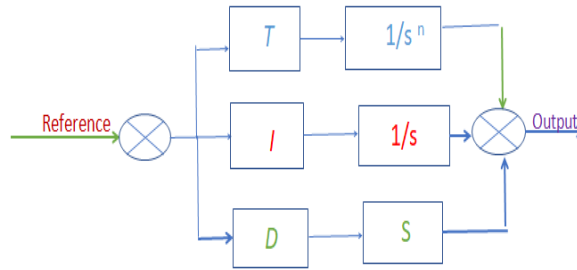


Figure 2. TID controller Block diagram

The TID controller surpasses a standard PID controller in terms of robustness, stability, flexibility, noise rejection, and adaptability. The TID controller offers significant advantages in certain applications, especially when dealing with complex system dynamics or when conventional PID control fails to meet performance criteria. Nevertheless, the efficacy of a TID controller is contingent upon the particular system and necessitates meticulous calibration and design[28-30].

A TID controller is particularly advantageous over a PID controller in systems where dead time is a significant factor. Its ability to handle delays directly, simplify tuning, and maintain stability in delayed systems makes it a preferred choice in such scenarios. However, for many other types of systems, especially those without significant time delays, a PID controller remains a versatile and widely used solution.

The gains are assigned within the maximum and minimum bounds, and the appropriate scaling parameter values are determined to limit or reduce the overall error function throughout the specified period. When constructing a modern controller using a heuristic optimisation approach, the objective function is first built with an emphasis on the suitable constraints and criteria. The objective function employed to enhance the effectuation of the suggested controller is the integral square error (ISE) criteria[31].

$$J = \int_0^{t_{sim}} ((\Delta f_1)^2 + (\Delta f_2)^2 + (\Delta p_{tie})^2) dt \quad (6)$$

Hence, the optimization issue can be formulated as the minimization of variable J, as depicted in equation 6. $K_{min} \leq K \leq K_{max}$. The range of values for n is between -2 and 2, with a minimum value of -2 and a maximum value of 2.

4. Cuttlefish Optimization Algorithm

The traditional Cuttlefish optimization method has been employed to optimize the process of extracting features, as explained in detail in this document. The COA method [32] is utilized as a search approach to determine the most exemplary subset of features. As depicted in Figure 3, the program replicates the physiological mechanisms by which cuttlefish modify their coloration. The observed patterns and hues in cuttlefish can be attributed to the phenomenon of light reflection from several layers of cells, namely chromatophores, leucophores, and iridophores. The analysis of the CFA focuses on two main processes: visibility and reflection. This study uses the reflection process to imitate the light reflection mechanism, while the visibility function is utilized to model the visibility of associated patterns.

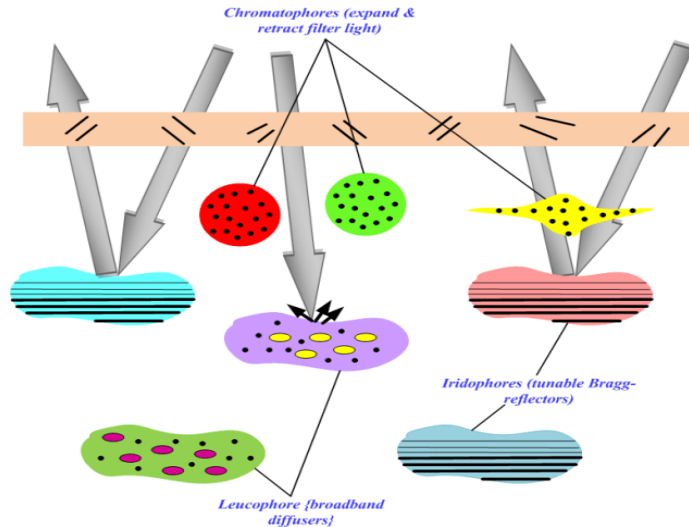


Figure 3. Cuttlefish Optimization Algorithm

Procedure for implementing the Cuttlefish Algorithm (CFA):

- *The conventional cuttlefish algorithm:*

Cuttlefish are marine creatures that are classified as molluscs. They possess an extraordinary ability to alter the colour and patterns of their skin in reaction to their environment. The interaction between chromatophores, leucophores, and iridophores within cells enables this result. By blending with the reflected light, these cells produce various colours and patterns.

- *Initialization:*

The technique utilizes a population of initial solutions composed of a subset of selected data points and a subset of unselected data points. When the subset of data points that were not picked is divided by the subset that was chosen, the resulting value should be zero. Each decision tree classifier calculates the fitness value for a selected subset of points in each pi of the subset. It is advisable to retain the subset of points that demonstrate a superior fitness value as both the optimal subset and the optimal subset of points. The optimal selection of data points should have a smaller dimension than the Avbest subset. Every starting solution is linked to an unselected subset of points and a selected subset of points. The goal is to determine the fitness value associated with each one initial solution of data values. An optimal arrangement of data points is used to develop and maintain the ideal arrangement of data points.

- *Feature selection:*

In the recent past, there has been a notable surge in the amount of data, resulting in the integration of a wide range of characteristics and attributes. As a result, the time it takes to perform the computation has been prolonged, resulting in the wastage of computational

resources, as most of these factors do not have any impact on the conclusion of a predictive model. Hence, it is customary to choose a subset of characteristics by considering the relative relevance of each variable, as shown by their separate weights, which have a more substantial influence on accurately forecasting the outcome. All other attributes are disregarded. CFA utilizes two unique processes, namely reflection and visibility, to identify a new and innovative solution. These examples perform a thorough search by using the significance of each point to determine a new area that encompasses the best solution within a specific range. Figure 4 displays the flowchart of the cuttlefish algorithm.

The methodology for determining the new solution (new P) by the use of reflection and visibility is outlined as follows.

The equation can be expressed as $P = \text{reflection} + \text{visibility}$.

The equation is $j = R * G1(i)$.

The visibility of points j is equal to $V * (\text{Best points } (j) - G1(i))$.

Where, G1 refers to a collection of cells. The variable R represents the measure of reflection.

The variable V represents the measure of visibility.

CFA Flow Chart:

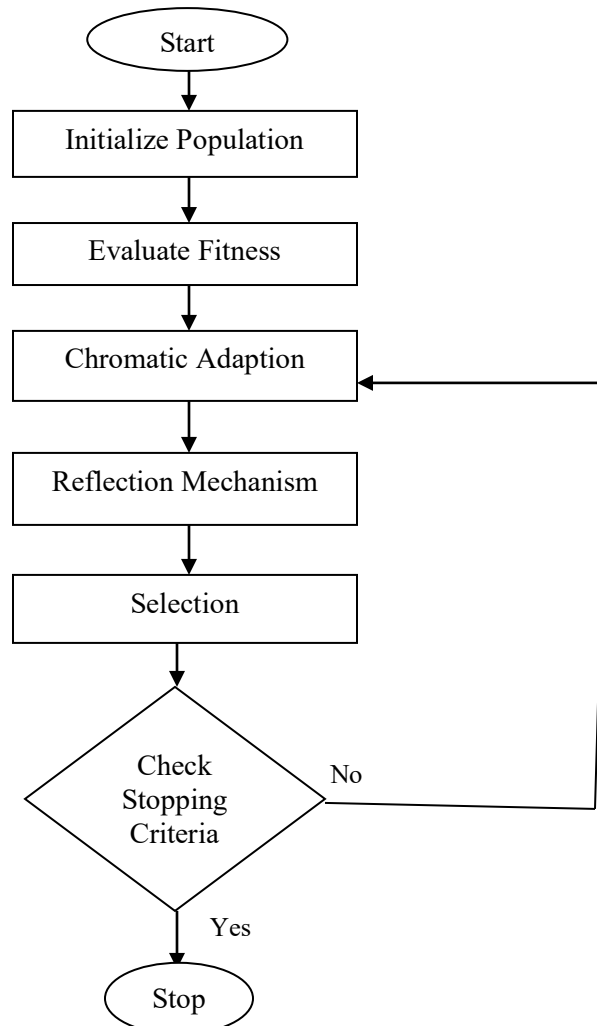


Figure 4. Flowchart of Cuttlefish Algorithm

Algorithm of the CFA:

- Step : 1 Define the Objective Function:
The goal is to minimize error in frequency and tie-line power deviation. The objective function as shown in Equ(6) is to be minimized.
- Step : 2 Generate Initial Population
The algorithm starts with a random population of controller parameters (e.g., Kt, Ki, Kd). As shown in Equ(5).
- Step : 3 Evaluate Fitness
Simulate the power system with those parameters and compute frequency and tie-line deviations. The fitness function measures how good the controller's performance is (less overshoot, faster settling time).
- Step : 4 Update Solutions
Reflection explores nearby solutions.
Visibility lets the algorithm jump to new regions if stuck in local minima.
Color changing adjusts the balance between exploration and exploitation.
- Step : 5 Select the Best Parameters
The algorithm iterates until it finds the optimal controller settings that ensure:
Fast frequency restoration, Minimum tie-line power oscillations and Robust performance under load changes.

5. Results and Discussion

Deregulation of the power system is an imperative requirement when assessing the most recent TID controller. In addition to linear components, nonlinear components GRC and GDB are assessed. Following this, a GRC threshold of 0.05 percent is enforced at some stage during the configuration procedure. GDB is more accurately defined as the replacement rate of the steam valve characteristic when torque is absent. A potential limitation of 0.06 percent arises when the GDB is incorporated.

Case 1: pool-co based transaction

A pool co-based transaction refers to the practice of redistributing the electricity load among power generation companies (GENCOs) in a certain region by distribution companies (DISCOs). The region's participation factor is established at 0.5 for an interval of four attributes that are deemed to be equivalent. Figures 5 (a), 5 (b), and 5 (c) illustrate the variations in frequency for area-1, area-2, and tie line power, respectively, while using various controllers based on COA and GWO. Table 1 illustrates that the performance of the COA-based controller is superior to that of the GWO-based controller when utilizing a pool co-based transaction.

$$APF = \begin{bmatrix} 0.5 \\ 0.5 \\ 0.5 \\ 0.5 \end{bmatrix} \text{Disco} = \begin{bmatrix} 0.1 \\ 0.1 \\ 0 \\ 0 \end{bmatrix} \text{p. u DPM} = \begin{bmatrix} 0.5 & 0.5 & 0 & 0 \\ 0.5 & 0.5 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Table 1. Comparison of distinct optimization controllers under case 1

S. No	% PO (p.u)			% PU (p.u)			ST (Sec)			ISE
	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	
GWO-PID [21]	0.005	0.004	-	0.058	0.062	-	5.6	5.4	5.4	0.076
COA-PID [22]	0.003	0.004	-	0.038	0.04	-	4.8	4.6	4.8	0.063
GWO-TID [25]	0.002	0.003	-	0.028	0.03	-	4.6	4.2	4.0	0.051
COA-TID (proposed)	0.001	0.003	-	0.022	0.028	-	4.2	3.8	3.7	0.038

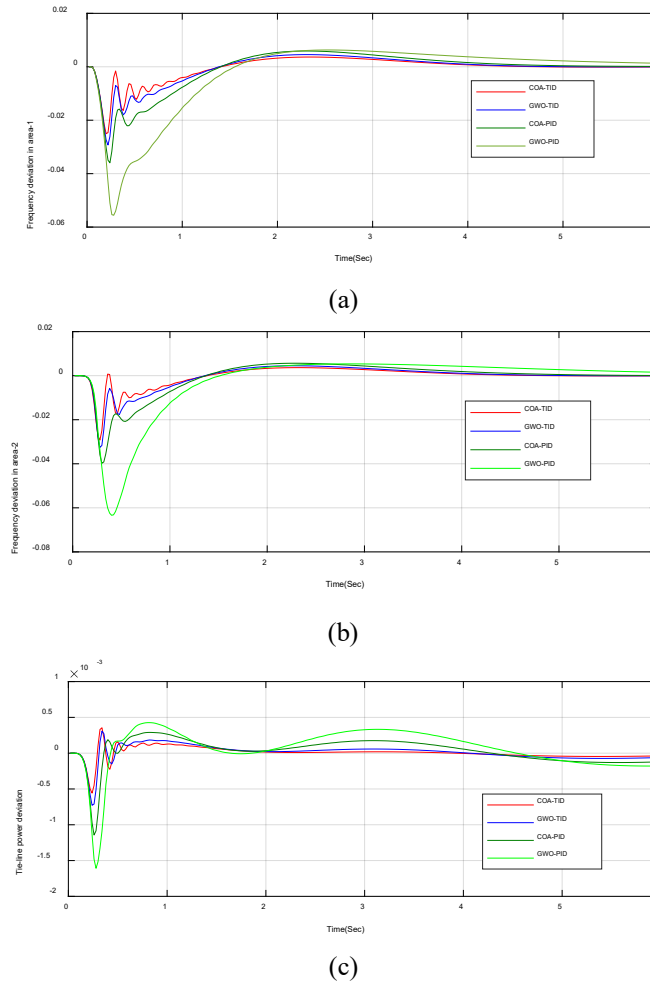


Figure 5. (a) Δf_1 , (b) Δf_2 , and (c) ΔP_{tie} for a 10% step load disturbance under case 1

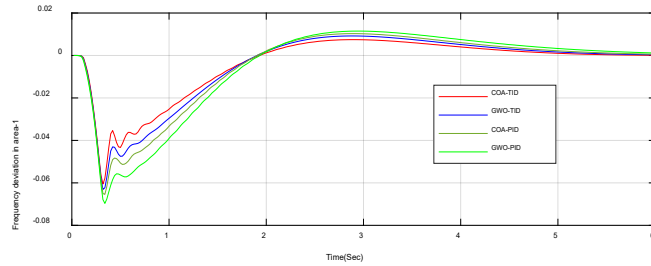
Case 2: Bilateral-based transaction

A bilateral based transaction refers to the sharing of the load between DISCOs and GENCOs in another area. Figures 6 (a), 6 (b), and 6 (c) depict the fluctuations in frequency in area-1, area-2, and tie line power, respectively. Table 2 illustrates that the COA-based controller exhibits superior performance compared to the GWO-based controller in bilateral transactions.

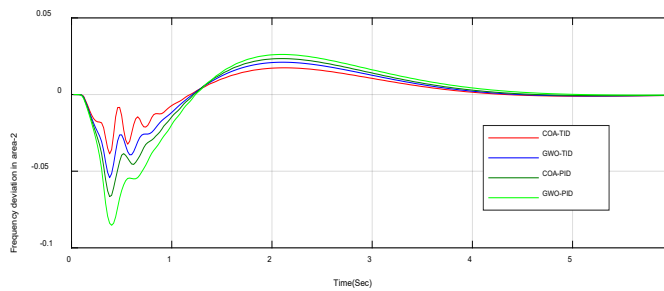
Table 2. Comparison of distinct optimization controllers under case 2.

S. No	% PO (p.u)			% PU (p.u)			ST (Sec)			ISE
	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	
GWO-PID [21]	0.01	0.003	-	0.07	0.08	0.035	5.6	4.8	5.2	0.056
COA-PID [22]	0.008	0.003	-	0.065	0.06	0.033	5.2	4.6	4.8	0.043
GWO-TID [25]	0.007	0.002	-	0.063	0.05	0.032	4.8	4.2	4.6	0.031
COA-TID (proposed)	0.005	0.002	-	0.06	0.03	0.03	4.6	3.8	4.2	0.026

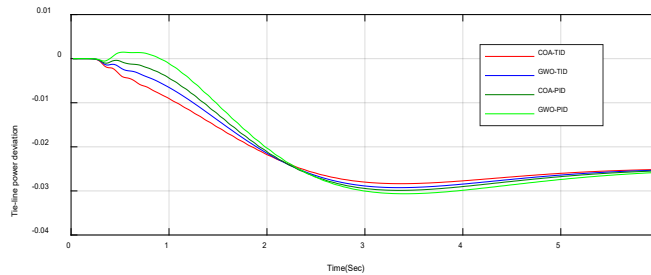
$$\text{APF} = \begin{bmatrix} 0.75 \\ 0.25 \\ 0.5 \\ 0.5 \end{bmatrix} \quad \text{Disco} = \begin{bmatrix} 0.1 \\ 0.1 \\ 0.1 \\ 0.1 \end{bmatrix} \quad \text{p. u DPM} = \begin{bmatrix} 0.5 & 0.25 & 0 & 0.3 \\ 0.2 & 0.25 & 0 & 0 \\ 0 & 0.25 & 1 & 0.7 \\ 0.3 & 0.25 & 0 & 0 \end{bmatrix}$$



(a)



(b)



(c)

 Figure 6. a) Δf_1 , (b) Δf_2 , and (c) ΔP_{tie} for a 10% step load disturbance under case 2.

Case 3: Contract violation

In this case, there is a violation of the contract as there is a request for excessive power above what is provided explicitly in the contract. Considering Case 2 once again, with the adjustment that DISCO1 requires an additional 0.1 (p.u. MW) of power. Figures 7(a) and (b) show the frequency deviation in area-1 and area-2, respectively. The variation of tie-line power is illustrated in Figure 7 (c) when various controllers based on COA and GWO are employed. Based on the results shown in Table 3, it can be observed that the COA-based controller exhibits superior performance in transactions pertaining to contract violations compared to the GWO-based controller.

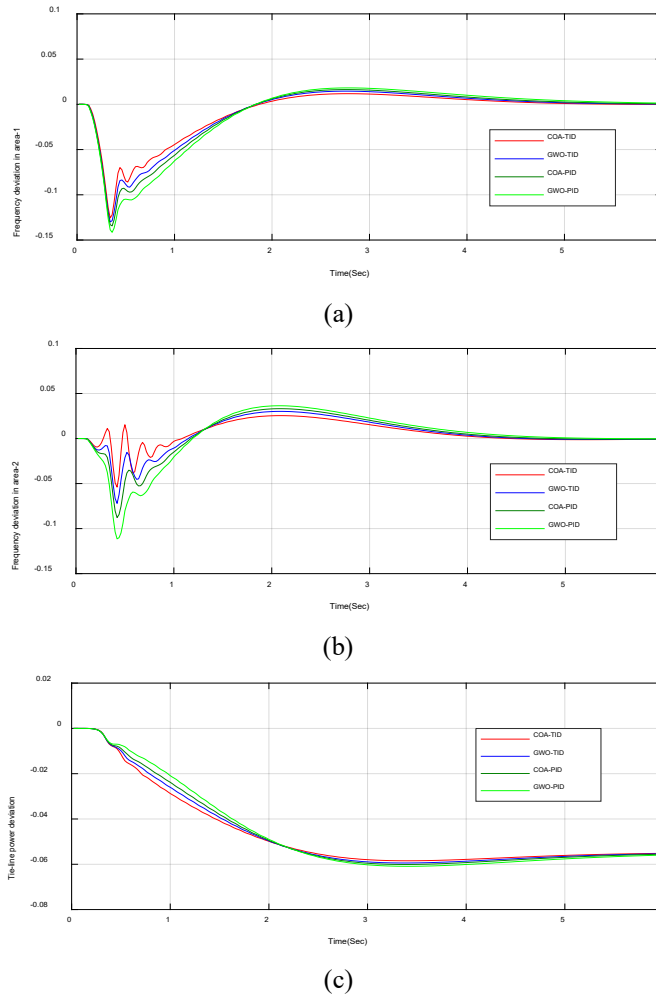


Figure 7. a) Δf_1 , (b) Δf_2 , and (c) ΔP_{tie} for a 10% step load disturbance under case 3

Table 3. Comparison of distinct optimization controllers under case 3

S. No	% PO (p.u)			% PU (p.u)			ST (Sec)			ISE
	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	
GWO-PID [21]	0.025	0.04	-	0.14	0.12	0.062	5.4	4.6	5.8	0.198
COA-PID [22]	0.024	0.03	-	0.13	0.08	0.060	4.8	4.4	5.4	0.136
GWO-TID [25]	0.022	0.02	-	0.12	0.06	0.058	4.6	4.2	5.2	0.111
COA-TID (proposed)	0.020	0.01	-	0.12	0.05	0.056	4.4	3.9	4.8	0.096

6. Conclusion

This study evaluates the effectiveness of the Tilt Integral Derivative (TID) controller in an open-market power system under different power transaction scenarios. The Cuttlefish Optimization Algorithm (COA) was employed to fine-tune the TID controller's parameters, and its performance was compared against the Grey Wolf Optimization (GWO) algorithm. Simulation results demonstrate that COA-tuned controllers consistently outperform GWO-tuned controllers, particularly in terms of faster settling times, reduced peak overshoot, and minimized peak undershoot across various loading conditions. Overall, the findings confirm that the COA-optimized TID controller provides superior frequency regulation compared to GWO-based tuning methods.

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